Production of Liquid Fuel Comparable to Commercial Grade Diesel by Pyrolysis of Waste High- Density Polyethylene Catalyzed with Portland Cement Using Single – Stage Semi– batch Reactor

Ahlam Al-Alas¹, Niyazi A. S. Al-Areqi¹, Elyas S. Alaghbari¹, Adeeb Al-Hatemi²

Abstract – Waste plastics constitute a growing social problem, because of the loss of natural resources, the environmental pollution, and the depletion of landfill space. In the present study, a Portland cement (PC) was used for the first time as very cheap and commercially available catalyst for the low– temperature pyrolysis of waste high – density polyethylene (WHDPE) to diesel range pyrolytic oil, utilizing a single – stage semi–batch reactor designed well at appropriate pyrolyzer / catalytic reformer ratio. The thermal decomposition of WHDPE was studied using a thermogravimetric analysis (TGA). The liquid fuel produced by catalytic pyrolysis of WHDPE at 250 °C were investigated by means of gas chromatography – mass spectrometry (GC–MS), Infrared (IR) spectroscopy, and physic–chemical properties of fuels. The PC–catalyzed pyrolysis resulted in remarkably increased liquid and gaseous products, and reduced char yield. Moreover, it significantly prevented the wax production. Moreover, this technique will contribute to address the problems related to the environmental protection from the accumulation of such waste plastics.

Index Terms— Catalytic pyrolysis, Liquid fuel, Waste plastics, WHDPE, PC, CG-MS.

1 INTRODUCTION

ASTE plastics constitute a growing social problem, because of the loss of natural resources, the environmental pollution, and the depletion of landfill space. The increased demand and consumption of virgin plastics have led in parallel to growing waste plastics disposed in landfills causing a serious danger towards the environment due to their slow degradation and subsequent contaminants generation. In other hand, the incineration of waste plastics emits severe air pollutants which also lead to environmental hazards [1-3]. Therefore. Many methods for recovering and recycling waste plastics have been developed. Among these with a view of the environmental protection and reduction of non-generation resources, a pyrolysis (thermal conversion of waste plastic to oils/fuels) have attracted a crucible interest worldwide [4-6]. There are four types of mechanisms of plastics pyrolysis, viz. end-chain scission, random-chain scission, chain stripping and cross–linking [7,8].

However, the conventional thermal pyrolysis suffers from certain limitations, such as high temperatures required [9], very broad product range with low yield % of produced liquid and gas fuels [10], and difficult decomposition of crossed chain polymers, *e.g.*, high– density, and low– density polyethylene (HDPE and LDPE) with polypropylene (PP) [11]. The catalytic pyrolysis has been developed to overcome such problems. Moreover, the use of catalyst can reduce the pyrolysis temperature, and also enhance the quality of the pyrolytic products in terms of desired range of carbon atom number and high energy efficiency[12–14].

Because of their simple design and easy operation, batch / semi–batch reactors have been used widely for the catalytic pyrolysis of plastics. But the *in situ* catalytic pyrolysis, in which the catalysts and plastic feedstock are in direct contact with each other in a single– stage batch reactor, has many drawbacks, such as low reaction rates, fast catalyst deactivation [14], and sophisticated catalyst recovery [15]. Such problems can however be resolved via *ex situ* catalytic pyrolysis by designing semi–batch reactors with a combination of sequential pyrolysis and catalytic reforming stages [16–21].

The war and conflicts going on in Yemen since the past five years have led to increasing prices of fuels by nearly ten orders of magnitude, *e.g.*, the diesel fuel, as well as the uncontrollable accumulation of garbage and waste plastics within the main streets of cities, particularly Taiz city which is still being blockaded till now. This has given us a motivation to conduct our research project on the catalytic pyrolysis of waste plastics for achieving that two–fold objective. In the present work, a Portland cement (PC) was used for the first time as very cheap and available catalyst for producing diesel range pyrolytic oil by the catalytic pyrolysis of waste high- density polyethylene (WHDPE) as one of the most abundant waste plastics in Yem-

 ¹ Department of Chemistry, Faculty of Applied Science, Taiz University, Taiz Yemen, Corresponding author E-mail:ahlamalals@gmail.com (A. Al-Alas), niyazi75.alareqi@gmail.com (N.A.S. Al-Areqi).

 ² Department of Industrial Chemistry, Faculty of Applied Science, Taiz University, Taiz Yemen, Corresponding author E-mail: adeebqassem2020@gmail.com (A. Al-Hatemi).

en, and has a large number of hydrocarbon groups, which are linearly chained. A single– stage semi– batch reactor made of stainless steel was designed in a cylindrical geometry with the overall capacity of 0.20 m³, so that pyrolyzer to catalytic reforming portion was maintained at the ratio of 3:1(Fig. 1).

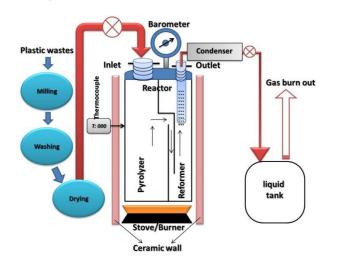


Fig. 1. Schematic of process and semi-batch reactor used for the catalytic pyrolysis.

2 MATERIALS & METHODS

A high–quality Portland cement (PC catalyst) was purchased from the local market supplied by the National Cement Company (NCC) – Hayel Saeed Anam & Co Ltd. (HAS), Lahij – Yemen. Finely ground powder of the PC catalyst was activated by pre–heating at 500 °C in a muffle furnace for 5 hrs.

Samples of WHDPE were collected from garbage sites and landfills located in several regions of Taiz city, Yemen. The WHDPE samples were milled into small pieces of 1.5 –2 cm size and thoroughly mixed. The resultant WHDPE pieces were washed using liquid detergent and water to remove any dirt or oils, and then dried under sun light.

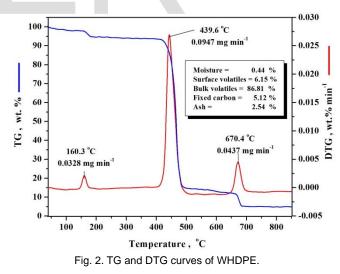
The catalytic pyrolysis experiments were carried out in a single- stage semi-batch reactor made of stainless steel as shown in Fig. 1 by packing the as- dried WHDPE pieces into the pyrolyzer upto the two thirds of its capacity. The activated PC catalyst (0.5 % with respect to the total WHDPE added) was then introduced to cover the bottom of catalytic reformer. The nitrogen gas was pumped into the tightly closed reactor for 15 min to displace the resident air prior to the pyrolysis. The reactor was thereafter heated gradually at a constant heating rate of 15 °C min-1. The pyrolytic liquid products were allowed to condensate out into a stainless steel container at fixed outlet temperature and pressure 250 °C and 2.5 bar, respectively maintained over whole the pyrolysis process. The gas products were burned out in air at the vent of the container to avoid the emission of hydrocarbon gases into the atmospheric environment. The yield % of each pyrolytic product (i.e., char, liquid, gas, and wax) was calculated after the completion of production based on the standard mass balance.

A Perkin Elmer thermal analyzer was used to investigate the thermal decomposition of WHDPE by means of simultaneous thermogravimetric– differential thermal (TG–DT) analysis applying a 15– mg dried WHDPE powder sample against α – alumina as a reference material. The instrument was run with 10 °C min⁻¹ heating rate and flowing a nitrogen gas from ambient temperature of 40 °C to 600 °C, and then air flowing upto 850 °C at a constant flow rate of 100 mL min⁻¹.

A Shimadzu–QP–2010 Ultra instrument with a flame ionization (FI) detector was employed to investigate the chemical composition of pyrolyzed liquid fuel by means of the gas chromatography coupled with mass spectrometry (GC–MS). An 1.0 μ L liquid sample was injected by a split mode into a HP–PONA capillary column (50 m × 0.25 mm i.d., 0.50 μ L thick). Helium of high purity was used as a carrier gas with a purge flow rate of 5 mL min⁻¹. The oven temperature was first set at 40 °C for 1 min, and it was thereafter increased upto 150 °C with a heating rate of 2 °C min⁻¹. The temperature of the ion source and interface were maintained at 200, and 250 °C, respectively. The chromatographic peaks were identified by means of the NIST mass spectral data library.

A Shimadzu IR spectrometer was also used to identify the functional groups of compounds present in the produced liquid fuels. IR spectra were scanned within the frequency range of $4000 - 400 \text{ cm}^{-1}$ with a spectral resolution of 4 cm⁻¹.

The high heating value, flash point, kinematic viscosity, and some other properties of liquid fuels were measured according to standard ASTM methods, considering three replications each.



3 RESULTS & DISCUSSION

TG and DTG curves of WHDPE (Fig. 2) show a clear two–step thermal degradation in the nitrogen atmosphere. The very low weight loss of the first step as 160.3 °C may be attributed to the elimination of short, defective polyethylene chains, which weakly bound to the surfaces of WHDPE particles. While the second high loss occurring at 439.6 °C is a clear evidence of the thermal history of the single step degradation of virgin polyethylene. Thus, the weight loss % of the first and second step were referred to the surface and bulk volatiles, respectively. The proximate analysis of WHDPE degradation is illustrated in the inset of Fig. 2. The moisture content was calculated from the weight loss % between ambient temperature and 150 °C. The ash content was equal to a constant weight % remaining after heating the sample at temperatures greater than 600 °C under air flowing. The fixed carbon was then computed using the mass % balance equation. It is interesting to note that the ash content and total volatiles play an important role in the production of liquid fuels by pyrolysis of waste plastics. The higher the ash content, the higher the production of gases and char, and the increase of volatile materials enhances the liquid yields.

The effect of the presence of PC– catalyst on the distribution of the product yields for WHDPE pyrolysis at 250 °C can be seen in Fig. 3. As expected, the PC– catalyzed pyrolysis resulted in remarkably increased liquid and gaseous products coupled with the reduction of char yield. Interestingly, the PC– catalysis also prevents the formation of wax. These results are well agreed with what have been reported for the catalytic pyrolysis of some waste plastics [11,22–24].

The GC–MS results of liquid fuel produced by the catalytic pyrolysis of WHDPE are illustrated in Fig. 4, and Tables 1. The last two hydrocarbons eluted at retention time (RT) of 44.14, and 48.70 min for the liquid fuel produced by the PC– catalyzed pyrolysis are tetracosane ($C_{24}H_{50}$), and 2,6,10,15-tetramethyl-heptadecane ($C_{21}H_{44}$) (Table 1).

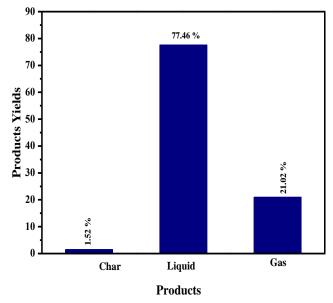
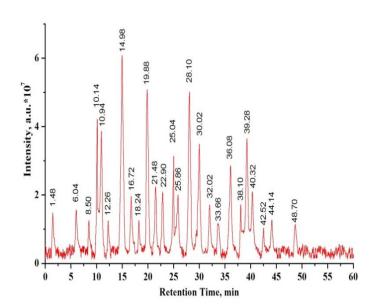
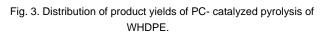


Fig. 4. GC-MS chromatogram of liquid fuels produced by PC- catalyzed pyrolysis of WHDPE.





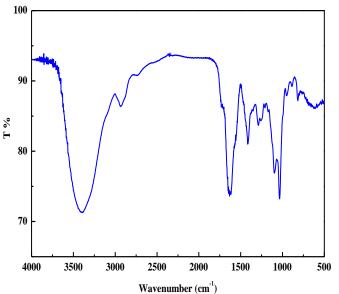


Fig. 5. IR spectrum of liquid fuel produced by PC- catalyzed pyrolysis of WHDPE.

Peak #	RT (min)	Peak area %	Trace Mass (m/z)	Name	Formula	MW	Prob%	NIST Lib #
1	1.48	1.01	81	Cyclopentene, 4,4-dimethyl-	C7H12	96	9.4	38642
2	6.04	1.02	81	Cyclohexene, 1-methyl-	C8H12	96	13.9	139432
3	8.50	0.83	67	1-Methyl-2-methylenecyclohexane	C8H14	110	24.3	113436
4	10.14	8.22	83	Cyclohexane, ethyl-	C8H16	112	44.6	113476
5	10.94	7.50	55	Cyclopentane, propyl-	C8H16	112	10.4	142655
6	12.26	0.91	43	Cyclohexanol, 2,4-dimethyl	C8H16O	128	14.4	114589
7	14.98	13.60	55	cis-2-Nonene	C9H18	126	16.3	113508
8	16.72	2.43	105	Cyclopentanol, 1-(1-methylene-2-propenyl)	C9H14O	138	11.8	152742
9	18.24	0.85	56	cis-3-Decene	C10H20	140	9.3	113558
10	19.88	11.20	56	3-Undecene, (Z)-	C11H22	153	8.2	142598
11	21.48	2.75	55	1,11-Dodecadiene	C12H22	166	11.5	6213
12	22.90	2.57	41	1-Tridecene	C13H26	182	14.2	107768
13	25.04	6.93	55	4-Tetradecene, (E)-	C14H28	196	9.3	142625
14	25.86	2.53	55	1-Tetradecene	C14H28	196	7.8	146721
15	28.10	11.35	55	1-Hexadecene	C16H32	224	16.7	118882
16	30.02	7.43	57	Octadecane	C18H36	254	17.2	57273
17	32.02	1.07	97	E-2-Octadecadecen-1-ol	C18H36O	268	7.4	131102
18	33.66	0.92	55	9-Nonadecene	C19H38	266	6.8	113627
19	36.08	3.19	57	Eicosane	C20H42	282	19.3	290513
20	38.10	1.05	57	Heneicosane (c.t.)	C21H44	296	36.6	107569
21	39.28	7.33	57	1-Docosene	C22H44	308	12.5	113878
22	40.32	2.72	57	Heneicosane	C21H44	296	16.8	107569
23	42.52	0.80	55	E-2-Docosene	C22H44	308	8.1	113879
24	44.14	0.83	57	Tetracosane	C24H50	338	15.7	248196
25	48.70	0.95	55	Heptadecane, 2,6,10,15-tetramethyl-	C21H44	296	10.4	14103

 TABLE 1

 LIST OF GC-MS IDENTIFIED COMPOUNDS PRESENT IN THE LIQUID FUEL OBTAINED FROM PC- CATALYZED PYROLYSIS OF WHDPE.

are assigned to stretching vibrations of C-CH3 and -CH2-, respectively. The strong wide band in the region 1700 – 1610 cm⁻¹ can be ascribed to the presence of C=O groups, while the shoulder apparent at ~ 1560 cm⁻¹ is due to the aliphatic C=C stretching vibrations. Although the GC-MS analysis showed on any carbonyl compound, the presence of C=O group in the liquid fuels under investigation as assigned by their IR spectra without a doubt arises from the pyrolyzed enols (Tables 1), which undergo a reversible tautomerization to carbonyl compounds [27]. The scissor vibrations of -CH2- and antisymmetric deformation of -CH₃ can be seen in the range of 1480 -1400 cm⁻¹. The short band at ~ 1230 cm⁻¹ is assigned to the C=C stretching vibrations and the two peaks at ~ 1100 and 1030 cm⁻¹ may be attributed to the different alcoholic and carbonyl C–O stretching vibrations. However, the three peaks at ~ 950, 880 and 815 cm⁻¹ are a clear evidence for the presence of

(cis) –CH=CH– and conjugated polyenes.

Based on the GC–MS results of the liquid fuels produced by PC– catalyzed and uncatalyzed pyrolysis of WHDPE, the distribution of pyrolyzed compounds in terms of their chromatographic peak area % as a function of cyclization, carbon number range, and saturation can be viewed in Figs. 6, 7, and 8, respectively. It is clear that the PC– catalysis leads to increased open– chain structures (Fig. 6), and a remarkable lowering of saturated compounds (Fig. 7) in the produced liquid. The interesting point to be emphasized here is that more than 37 % of hydrocarbons produced by the catalytic pyrolysis have a carbon range of the kerosene (C11–C17). followed by C18– C24, as much as 26.20 %.

Values of characteristic parameters of liquid fuels obtained from the catalytic pyrolysis of WHDPE are summarized in Table 2. It can be observed that the properties measured for the produced liquid fuel of the PC– catalyzed pyrolysis significantly match well with 26.20 % (Fig. 8). This indicates that, to a great extent, the liquid fuel pyrolyzed by the PC– catalysis approaches the composition of conventional diesel [28–30]. These results suggest that the PC–catalyzed pyrolysis of WHDPE follows the free– radical mechanism proposed by Sekine and Fujimoto for the pyrolysis of PP catalyzed with the Fe–activated carbon [31].

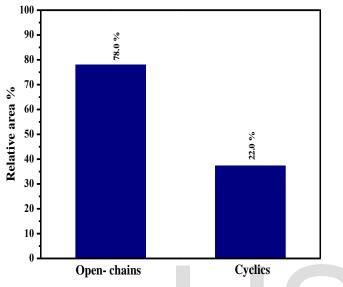


Fig. 6. Distribution of open- chain and cyclic compounds of liquid fuel produced by catalytic pyrolysis of WHDPE.

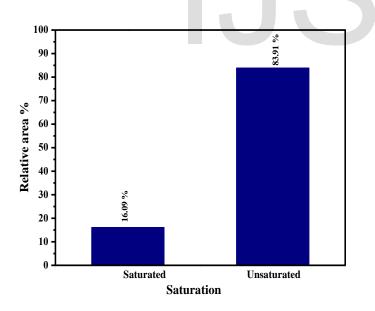


Fig. 7. Distribution of saturated and unsaturated compounds of liquid fuel produced by catalytic pyrolysis of WHDPE.

Values of characteristic parameters of liquid fuels obtained from the catalytic pyrolysis of WHDPE are summarized in Table 2. It can be observed that the properties measured for the produced liquid fuel of the PC– catalyzed pyrolysis significantly match well with the GC–MS results revealed earlier. Interestingly, These parameters measured for liquid fuel under investigation fall within the acceptable ranges reported for the conventional diesel [9,21,32]. Therefore, the results obtained in the present study prove that the low– temperature pyrolysis of WHDPE catalyzed with a low–cost Portland cement can potentially be used for producing high– yield liquid fuels comparable to the commercial grade diesel.

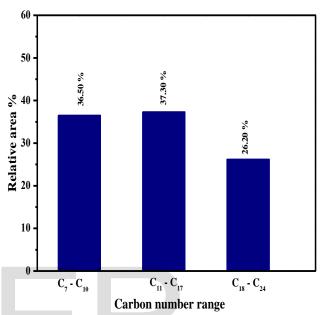


Fig. 8. Distribution of carbon number ranges for compounds of liquid fuel produced by catalytic pyrolysis of WHDPE.

TABLE 3 PROPERTIES OF LIQUID FUEL PRODUCED BY PC- CATALYZED PYROL-YSIS OF WHDPE.

Properties	Unit	Catalytic	Test method
		pyrolysis	
High heating value	MJ/kg	46.65	ASTM D 240
Flash point	٥C	39.5	ASTM D 93
Fire point	٥C	44.5	-
Cetane index	-	49	ASTM D 976
Carbon residue	wt %	0.280	ASTM D 189
Moisture content	wt %	0.305	ASTM D 95
Density @ 20 °C	kg/m³	843.2	ASTM D1298
Kinematic viscosity @ 40 °C	cSt	2.43	ASTM D 445

4 CONCLUSION

The use of very cheap and commercially available Portland cement along with the simple semi–batch reactor designed well at appropriate ratio of pyrolyzer and catalytic reformer feasibly allowed the low– temperature production of high– yield liquid fuel from the WHDPE pyrolysis. The hydrocarbon composition and functional properties of the liquid fuel produced by the PC–catalyzed pyrolysis were found to be similar to what have been reported for the commercial grade diesel. It can be concluded that the use of the produced liquid fuel as a substitute of , or blended with the conventional diesel, besides other products (gas and char) having a variety of promising applications, would essentially enhance the economic viability of the catalytic pyrolysis of waste plastics. Moreover, this will contribute to address the problems related to the environmental protection from the accumulation of such waste plastics.

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